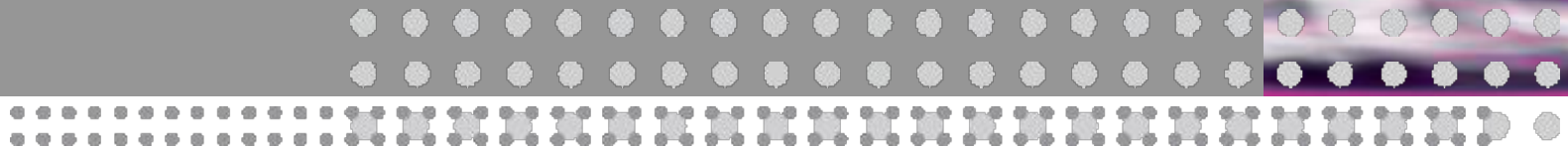
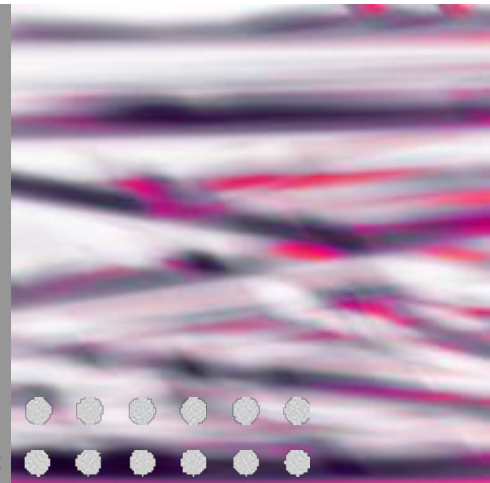


Raman Amplification for Telecom Optical Networks



Dominique Bayart

Alcatel-Lucent Bell Labs France, Research Center of Villarceaux

Training day www.Brighter.eu project

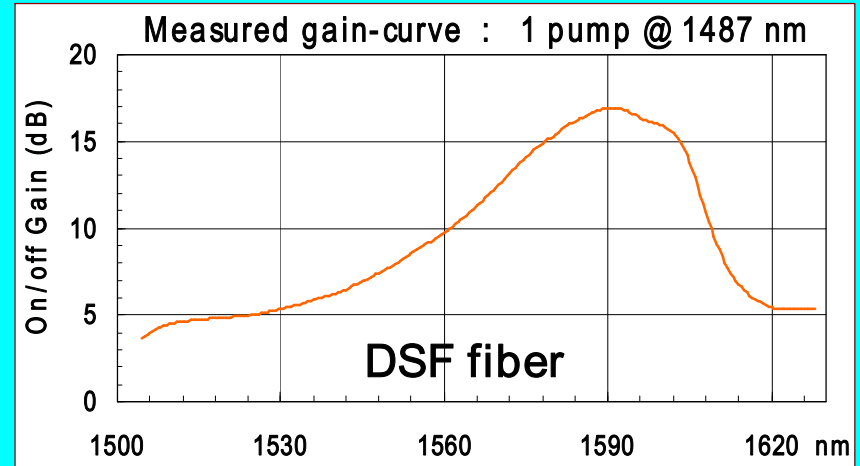
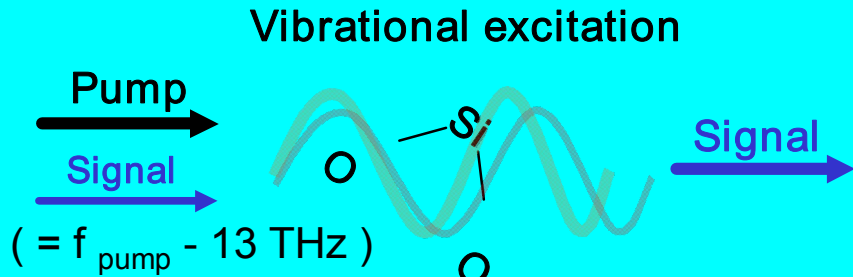
Cork, June 20th 2008

Raman Amplification for Telecom Optical Networks

Outline of the talk

- Raman interaction of Light with the glass
- Spectral and power characteristics
- Noise performance and limitations
(Rayleigh, noise transfer)
- System implementation
- Lumped Raman amplifiers

Raman amplification : Principle



$$G_{ON/OFF}^{dB} = \frac{10}{\ln 10} \cdot \frac{g_r}{A_{eff}} \cdot \frac{1 - e^{-\alpha_p \cdot L}}{\alpha_p} \cdot P_p$$

A_{eff} is the Raman effective area of the fiber

L_{eff} : Effective length of the fiber expressed as :

$$L_{eff} = \frac{1}{\alpha_p}$$

Effect happens for any pump frequency, polarization dependent

Instantaneous effect (not the travel time of the pump along the fiber !)

Peak Raman shift = - 13 THz (glass phonon energy)

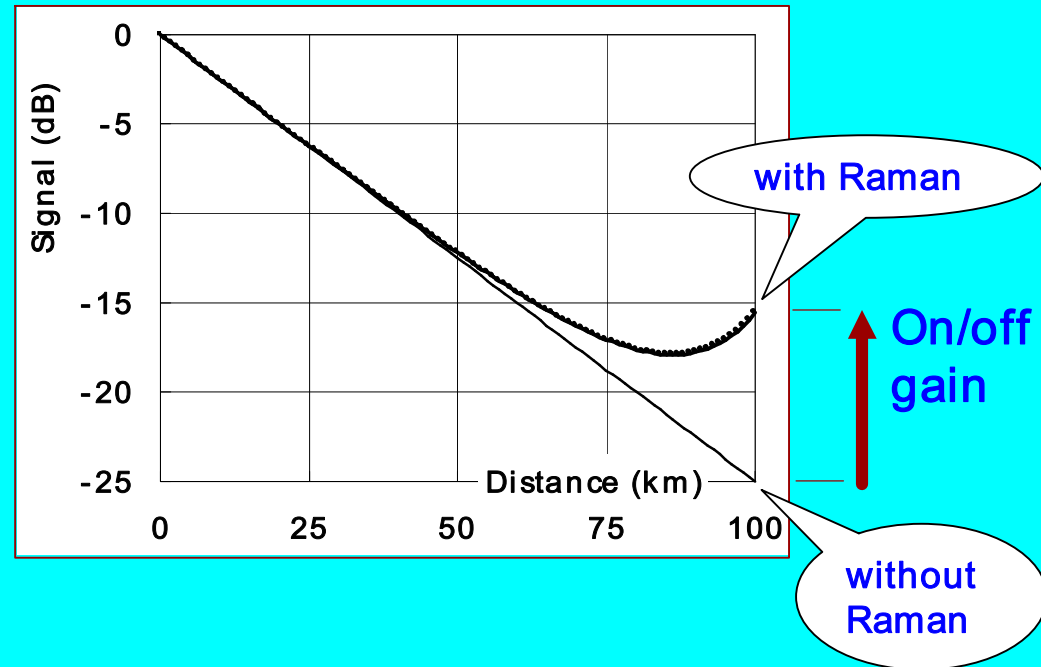
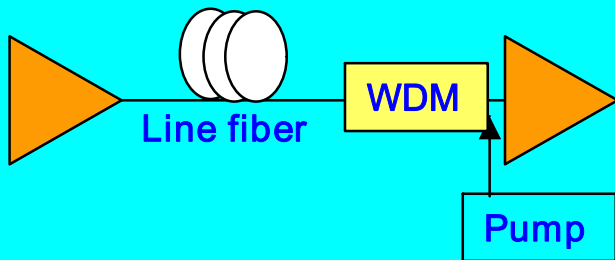
Top width = 2.5 THz, can be broadened with multi- λ pumping

→ Long interaction fibers

→ Confinement

→ Attenuation at the pump wavelength is paramount

Distributed Raman Pre amplification

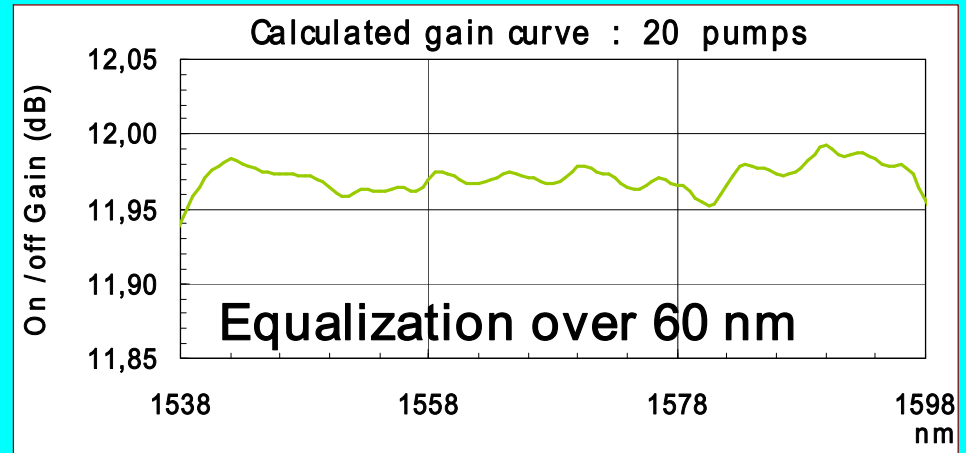
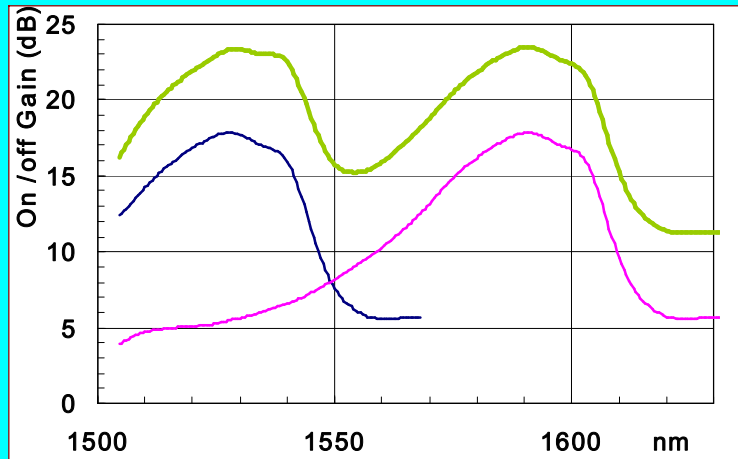


Pre amplification (backward pumping : weak gain saturation)

Increase of the signal powers at the EDFA input

(improved signal to noise ratio)

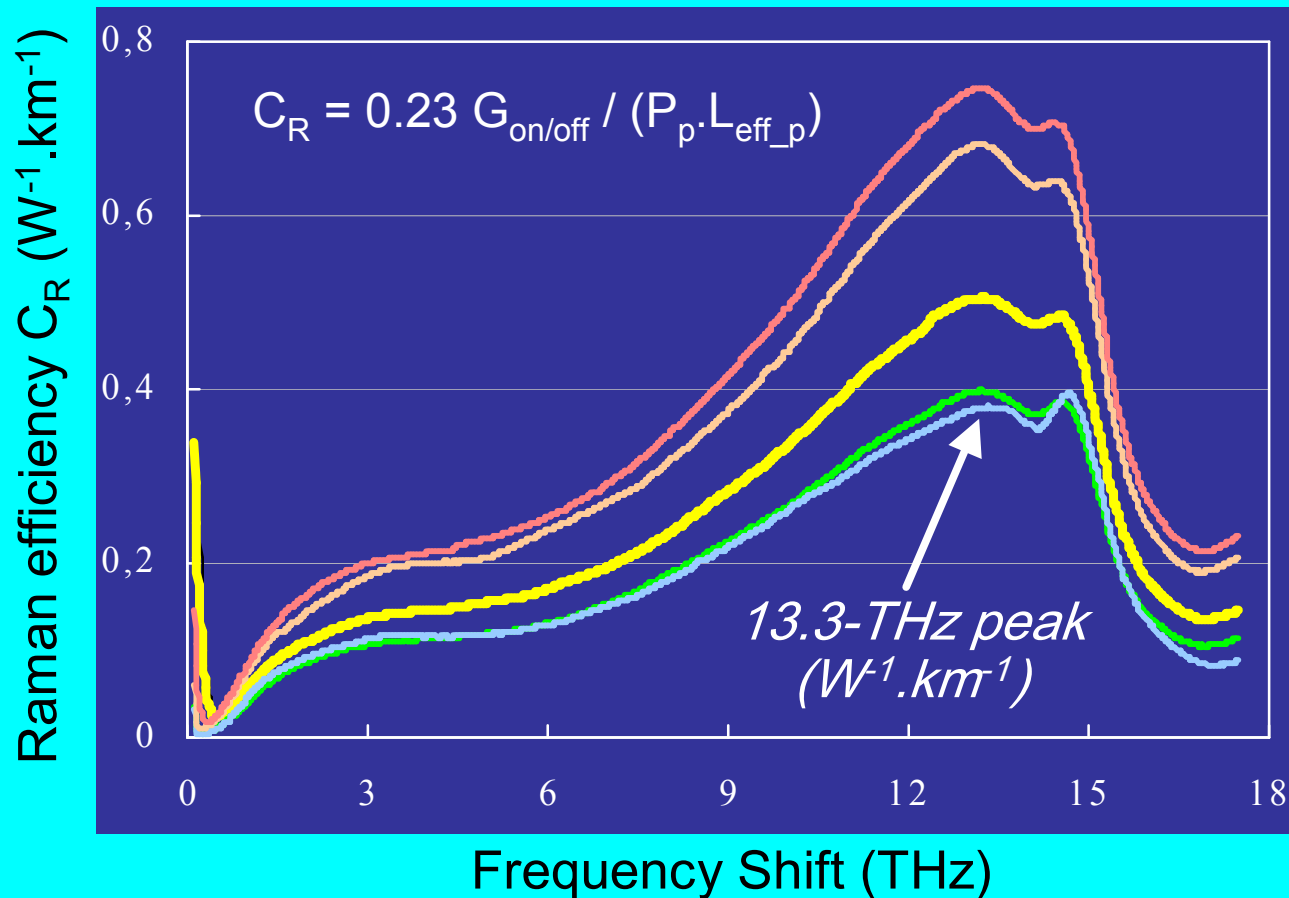
Pump wavelength combination



- ✓ 2 or 3 wavelengths enough for a 1-dB equalization over the C-band
- 3 to 4 over the C+L band
- Semiconductor pumps need polarization multiplexing or depolarization using PANDA fiber at 45 deg.

Fiber efficiency per unit length and per W of pump

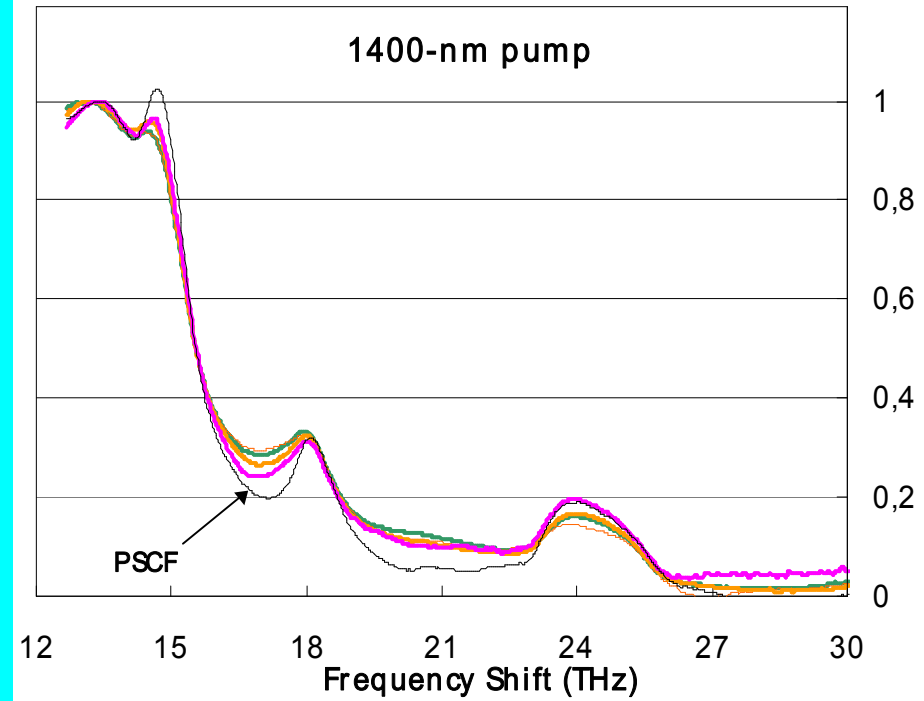
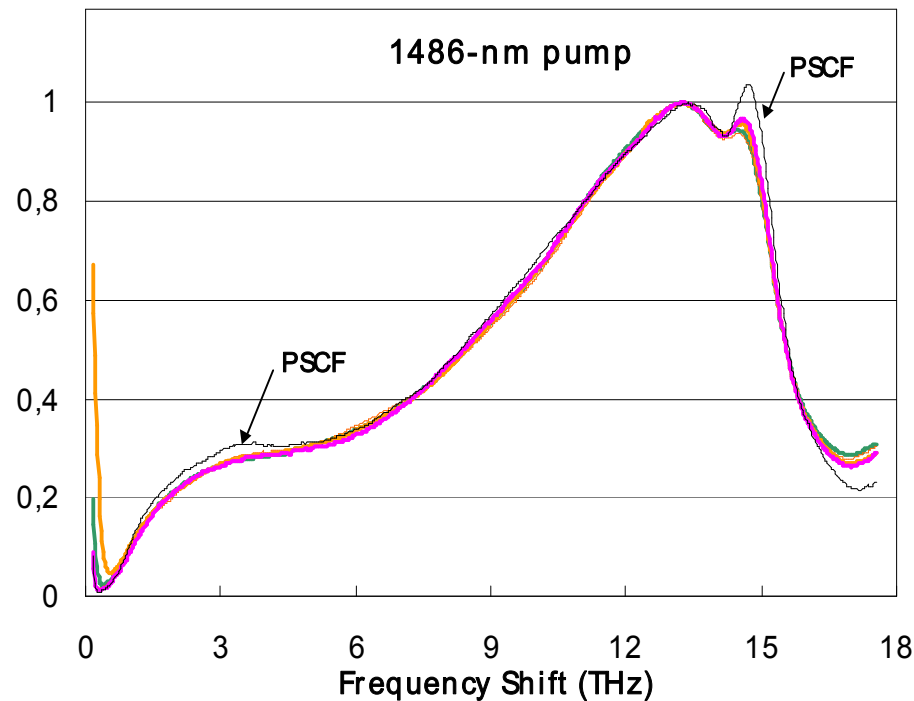
1486-nm pumping



| | C_R Max |
|-----------|-----------|
| NZDSF+ | 0.75 |
| NZDSF- | 0.68 |
| TeraLight | 0.51 |
| SMF | 0.40 |
| PSCF | 0.38 |

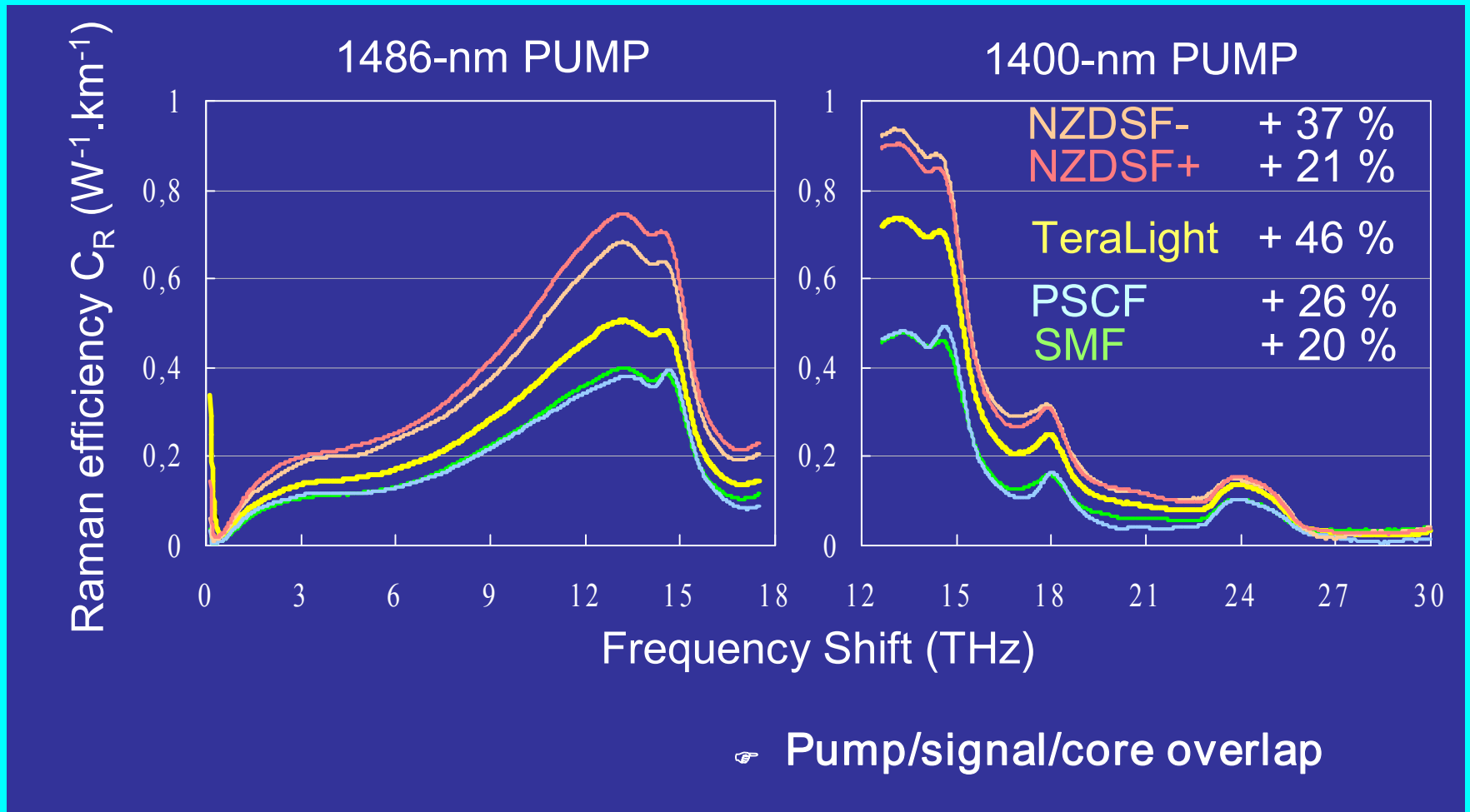
Normalized Gain Spectra

CURVES NORMALISED RELATIVE TO 13.3-THz PEAK

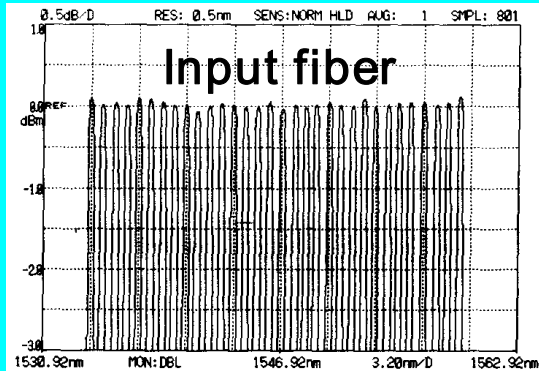


Boson-peak relative-intensity higher with SiO_2 than with GeO_2
13.3-THz peak : Ge-dependent, extends up to > 20 THz
Sharp 14.5-THz and 18-THz peaks specific to SiO_2

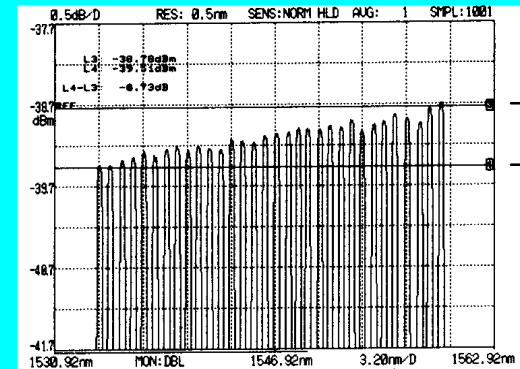
Fiber efficiency is pump wavelength dependent



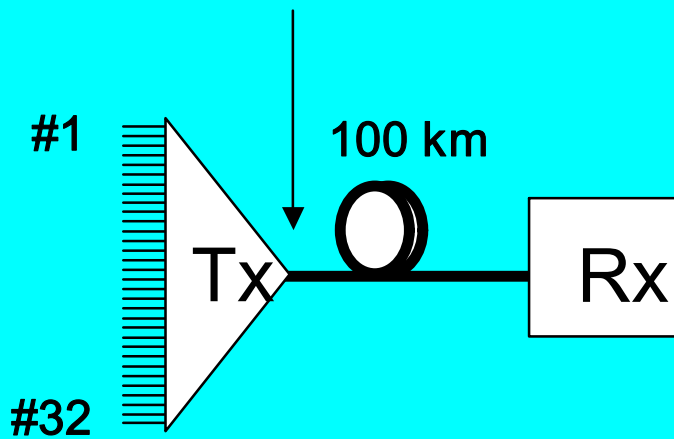
Effect of interchannel Raman depletion



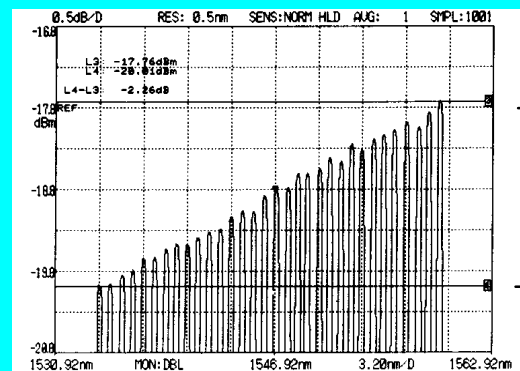
-10 dBm /channel
(linear regime)



0.7 dB

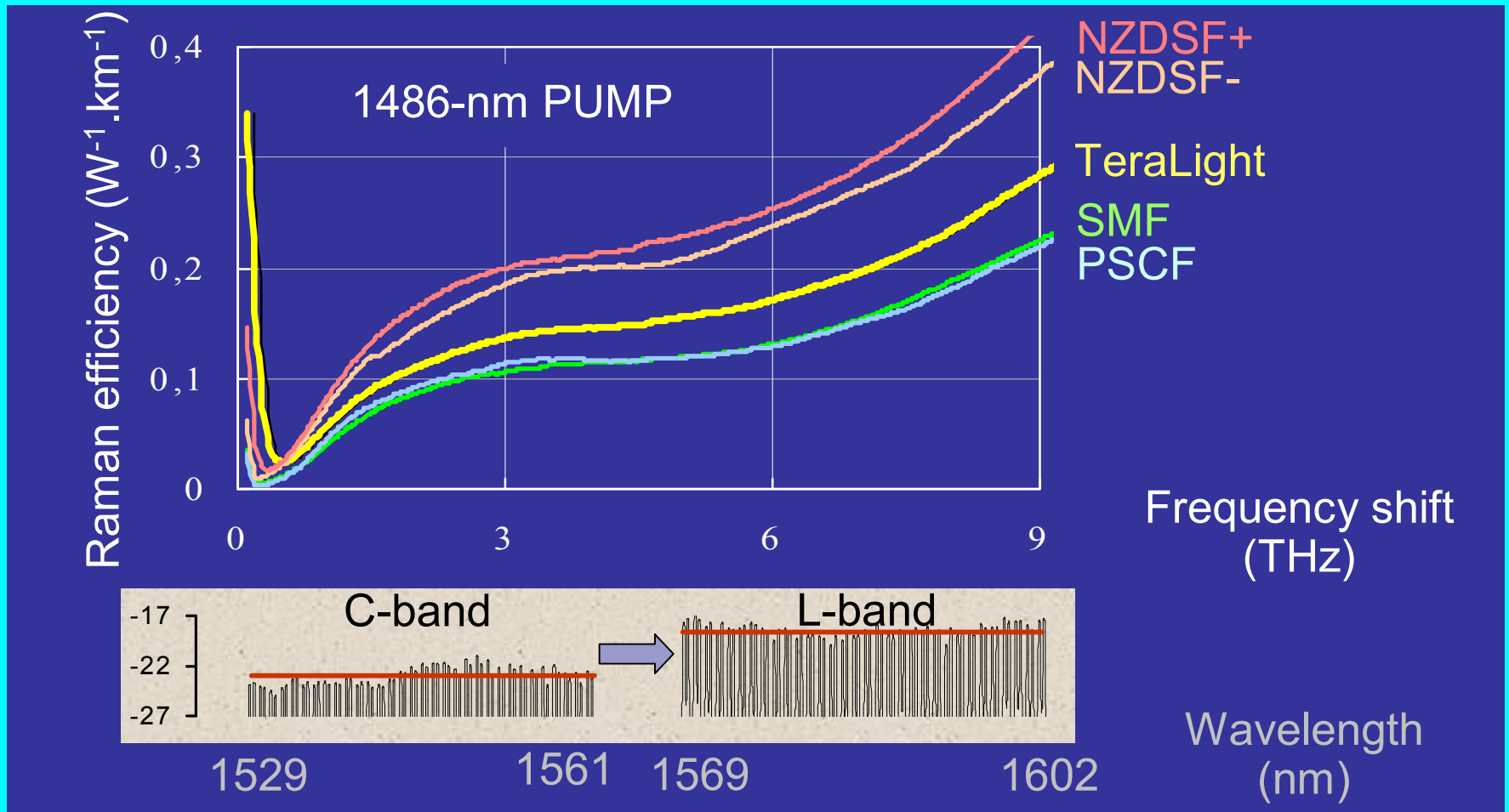


5.6 dBm /ch.

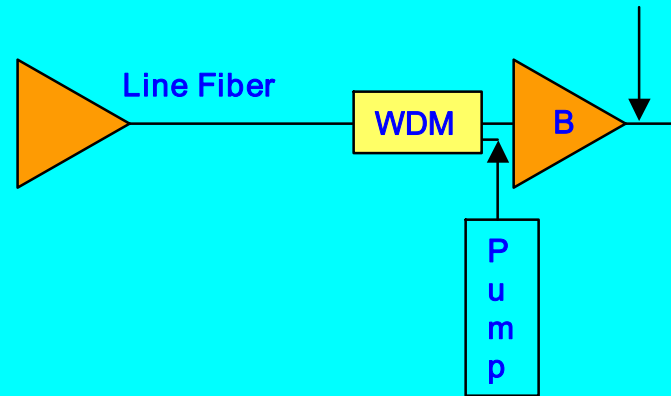


2.3 dB

Small-frequency-shift energy transfers



Noise figure for Distributed Raman Pre-amplification

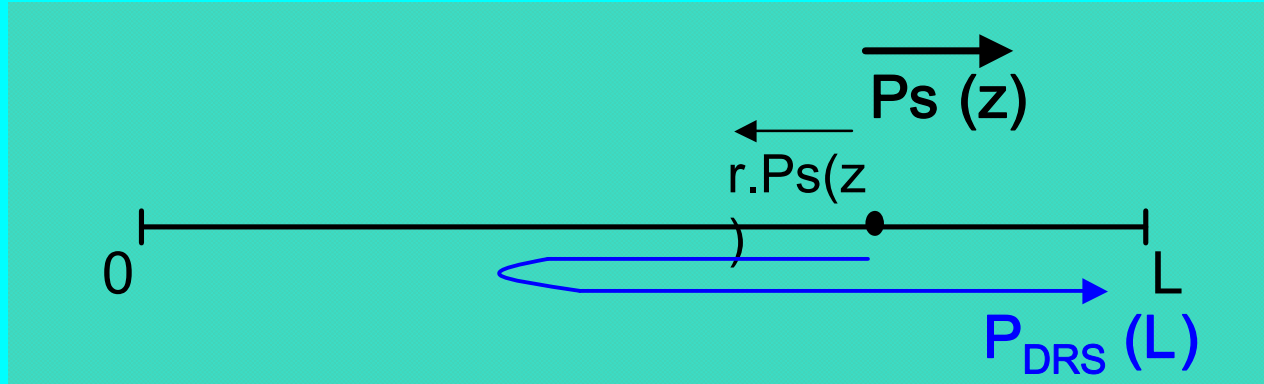


Intrinsic noise parameter = 3dB (quantum limit)

Equivalent noise figure = *the noise figure of an EDFA located in B point and providing with the Raman ON/OFF gain*

Equivalent noise figures can be equal or lower than 0 dB

Double-Rayleigh Scattering



- Signal (neglecting the DRS term): $P_S(z) = P_S(0) \cdot G_{net}(0 \rightarrow z)$
- Simple Rayleigh-scattered signal: $P_{RS}(y) = \int_y^L r \cdot P_S(z) \cdot G_{net}(y \rightarrow z) \cdot dz$
- Double Rayleigh-scattered signal: $P_{DRS}(L) = \int_0^L r \cdot P_{RS}(y) \cdot G_{net}(y \rightarrow L) \cdot dy$

⇒ DRS noise-to-signal ratio at the end of the fibre:

$$R_{DRS} =$$

$$P_{DRS}(L)/P_S(L)$$

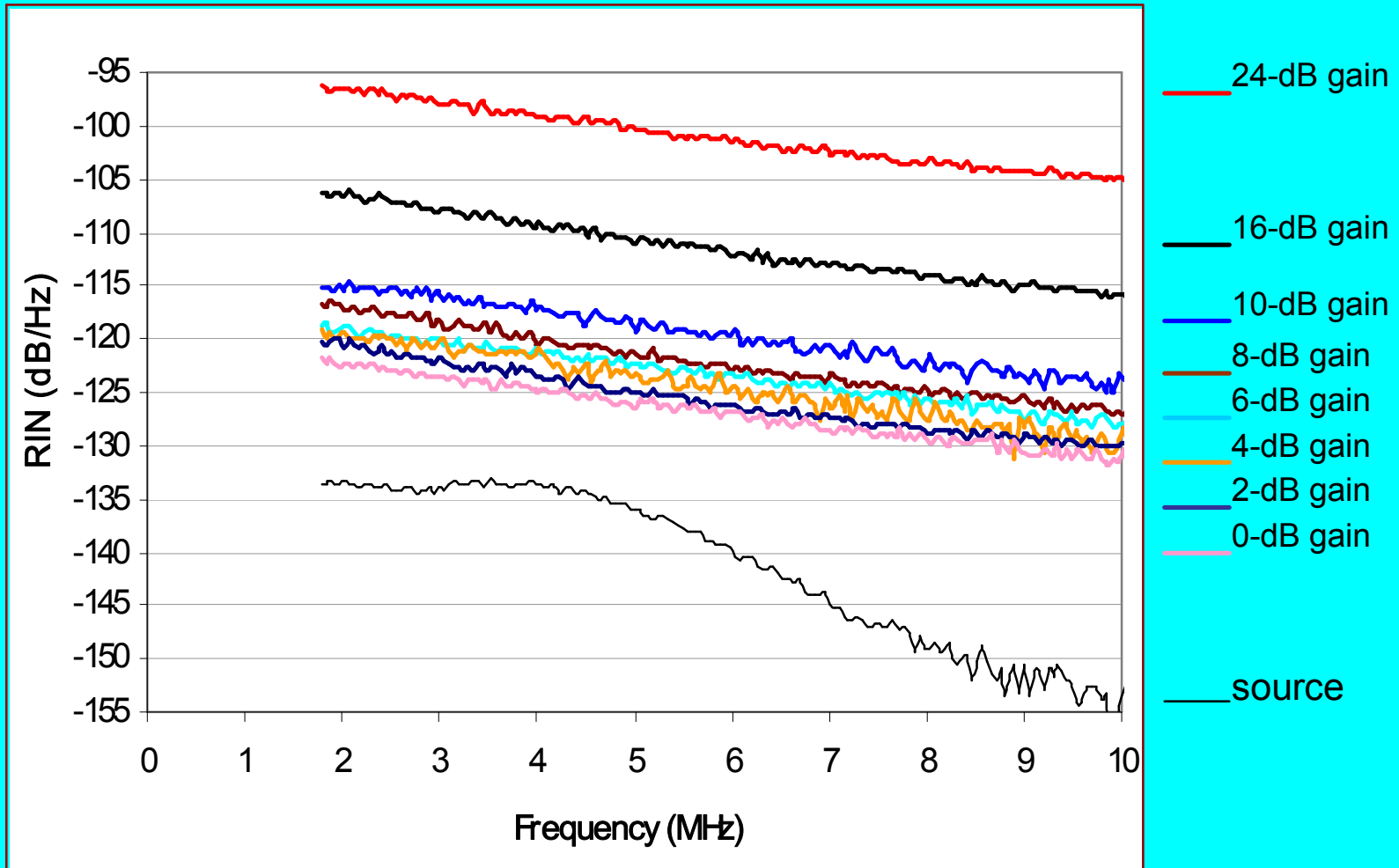
Double-Rayleigh Scattering (DRS)

- DRS is a delayed copy of the signal => beating noise at detection with the signal by quadratic detection:

$$RIN(f) \approx R_{DRS} \frac{2}{\pi} \frac{\Delta\nu}{(f^2 + (\Delta\nu)^2)}$$

- Exists in all transmissions but is more penalizing with distributed Raman amplification: DRS is amplified during its double-path
- Crucial issue: DRS impairment is a limit to high amounts of Raman gain
- ASE and DRS essentially differ by their spectral distribution:
 - ASE is constant with wavelength in the range of the signal bandwidth
 - DRS is a replica of the signal optical spectrum

Electrical measurement of DRS



Signal-ASE and signal-DRS beat noises

- Reference case:
NRZ, broad optical filtering

$$\sigma_{\text{sg-ASE}}^2 = 4\eta^2 N_{\text{ASE}}^{\text{sg polar}} P_S B_{\text{elec}}$$

$$\sigma_{\text{sg-DRS}}^2 = 2\eta^2 P_{\text{DRS}}^{\text{sg polar}} P_S$$

- General case:
any format

$$\sigma_{\text{sg-ASE}}^2 = k_{\text{ASE}} \cdot P_{\text{ASE}} P_S$$

$$\sigma_{\text{sg-DRS}}^2 = k_{\text{DRS}} \cdot P_{\text{DRS}} P_S$$

depend on:

- modulation format (signal pattern)
- optical and electrical filters at reception

Conclusion on Double-Raleigh Scattering

DRS is a major limitation of the maximum Raman gain that can be obtained in the line fiber

Limits Raman advantage in backward pumping

Max gain closed to 23 dB

For all Raman pumping of the line fiber

Need for forward pumping

- ✓ See related issues (RIN, ...)

Or use of Raman pumping into the DCF

- ✓ Increases non-linear effects in the DCF

Pump-to-signal RIN transfer

Raman effect is very fast (femtosecond)

Locally, the intensity fluctuations of the pump are totally transferred to the signal by gain (dB)

Effect averaged

- by counter propagation (backward pumping)
- only by chromatic dispersion for forward pumping

Transfer functions

Assumptions:

Distributed Raman amplification: long fiber (50 -100km)

Moderate Raman gain, moderate pump RIN

No pump depletion

$$RIN_S(f) = RIN_P + 20 \log \left[\frac{\langle G_{ON/OFF} \rangle}{10 / \ln(10)} \right] - 10 \log \left[1 + \left(\frac{f}{f_c} \right)^2 \right]$$

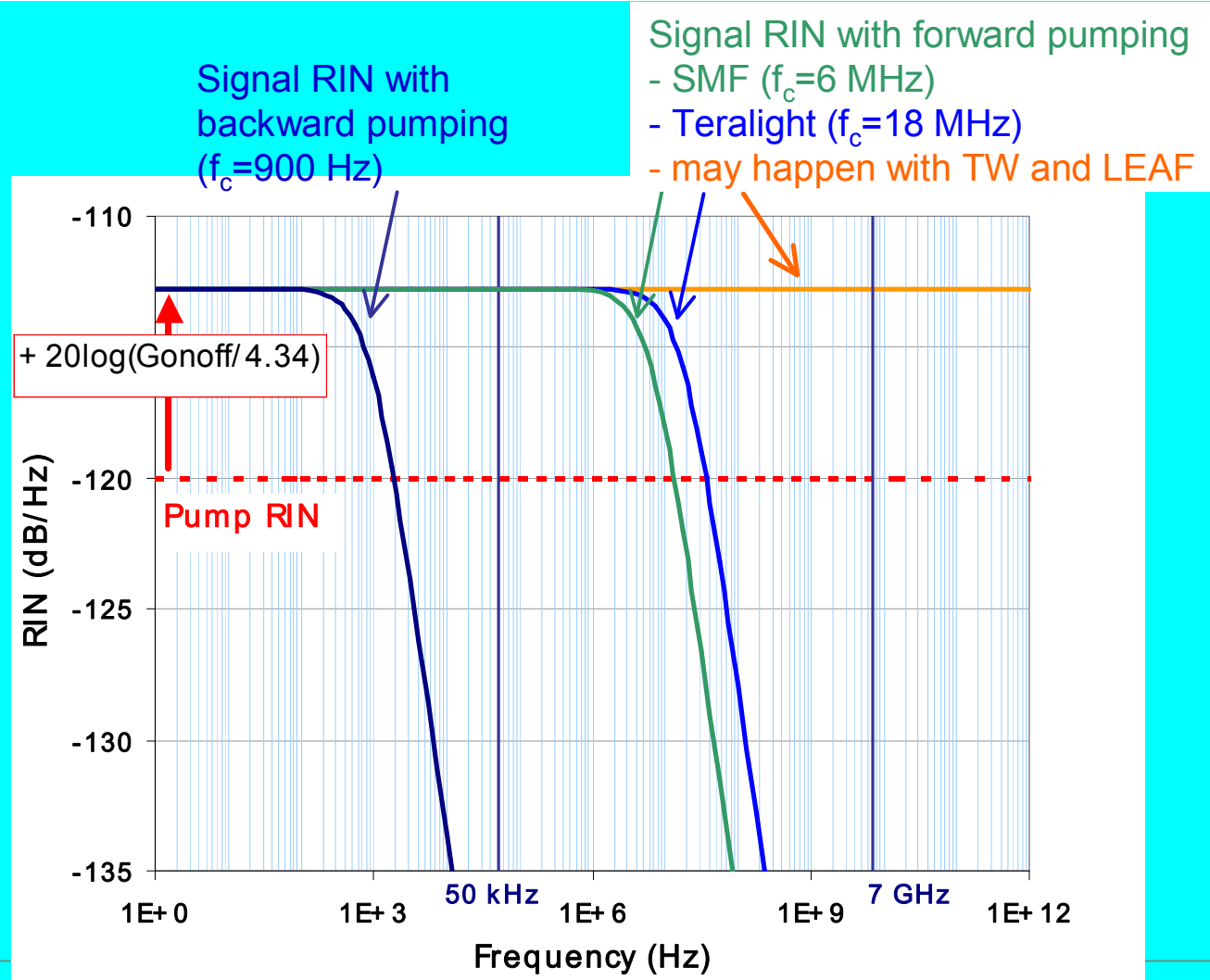
$$\text{with } f_c = \frac{\alpha_P V_S}{4\pi} \text{ for backward pumping}$$

$$\text{and } f_c = \frac{\alpha_P}{2\pi \left(\frac{1}{V_S} - \frac{1}{V_P} \right)} \text{ for forward pumping}$$

Reference: C. R. S. Fludger and al., Electron. Lett., 2001, 37, (1), pp. 15-17

Transfer functions

With:
 $RIN_p = -120 \text{ dB/Hz}$
 $G_{\text{onoff}} = 10 \text{ dB}$
 $\alpha_p = 0.25 \text{ dB}$
 $\lambda_p = 1450 \text{ nm}$
 $\lambda_s = 1550 \text{ nm}$



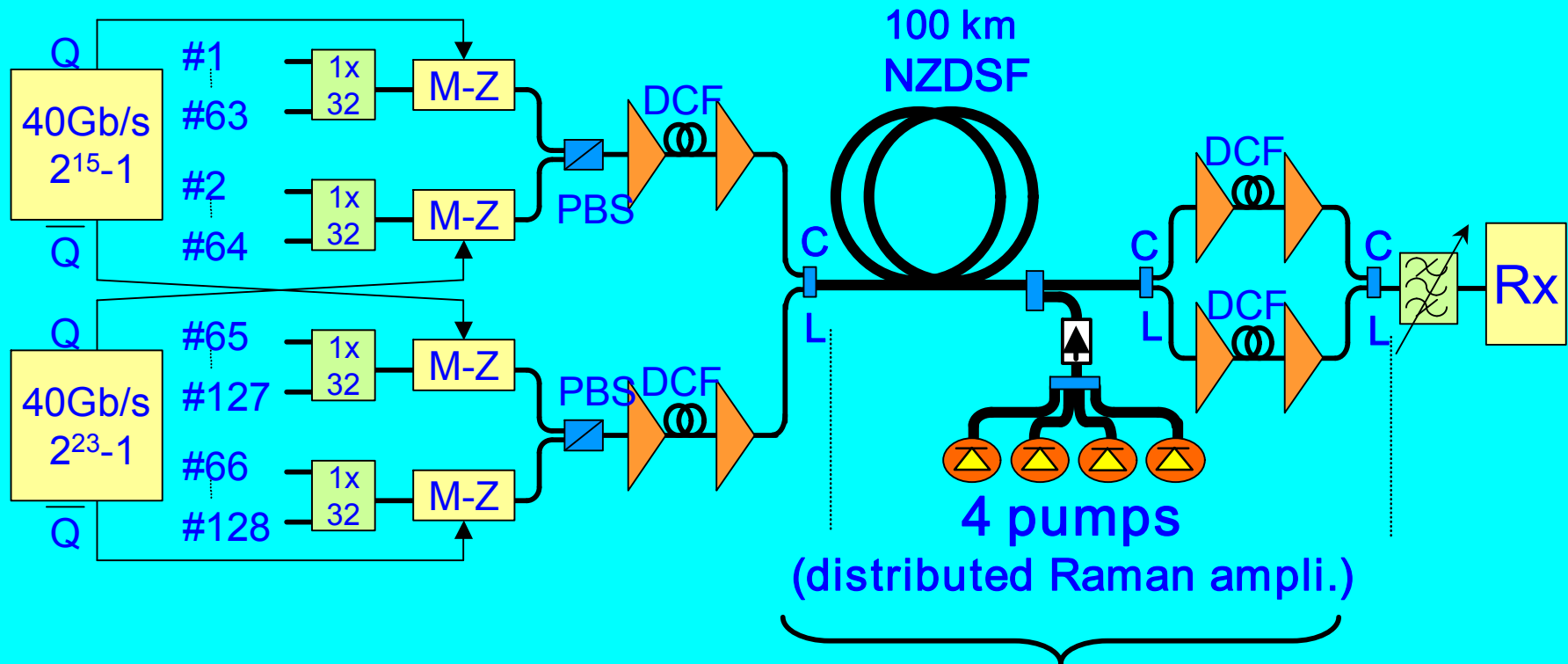
Signal RIN with forward pumping
 - SMF (f_c=6 MHz)
 - Teralight (f_c=18 MHz)
 - may happen with TW and LEAF

Signal RIN with backward pumping (f_c=900 Hz)

+ 20log(Gonoff/4.34)

Pump RIN

Raman amplification : Implementation



Use of wavelength multiplexed Raman pumps $\times 3$

Efficiency depends on fiber type and characteristics

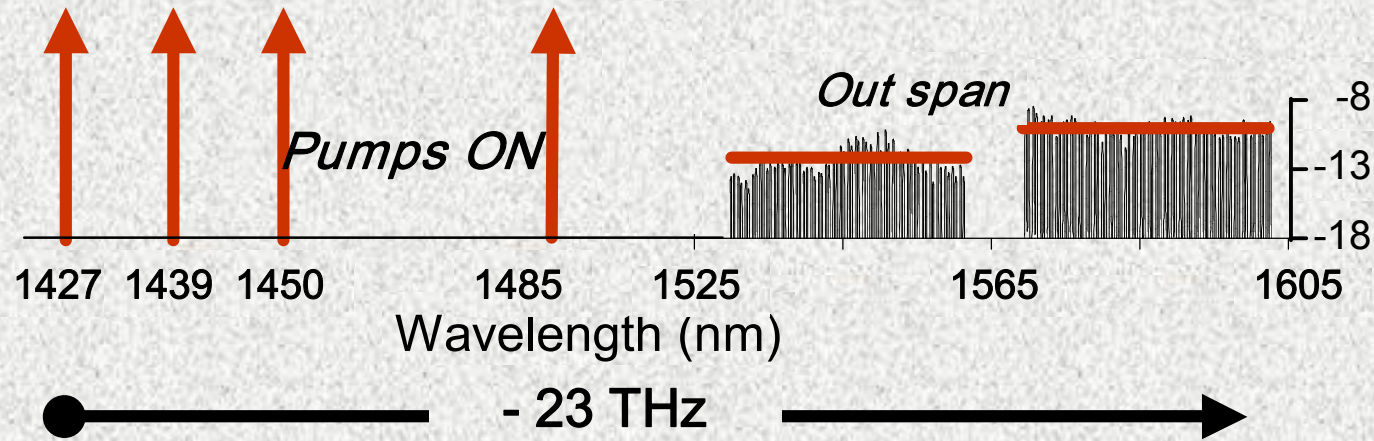
Stimulated Raman Scattering



Pumps OFF



Intraband-tilt compensated but C-to-L energy-transfer

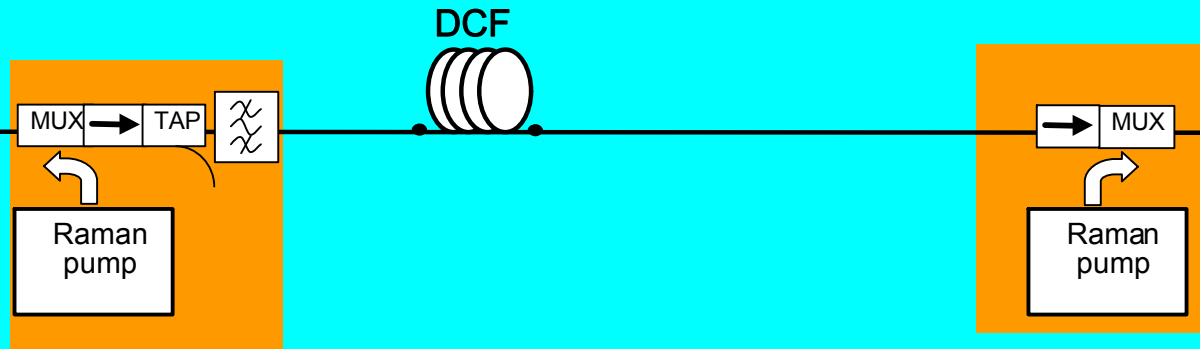


Raman gain
 12dB C-band
 10dB L-band

All Raman pumping schemes

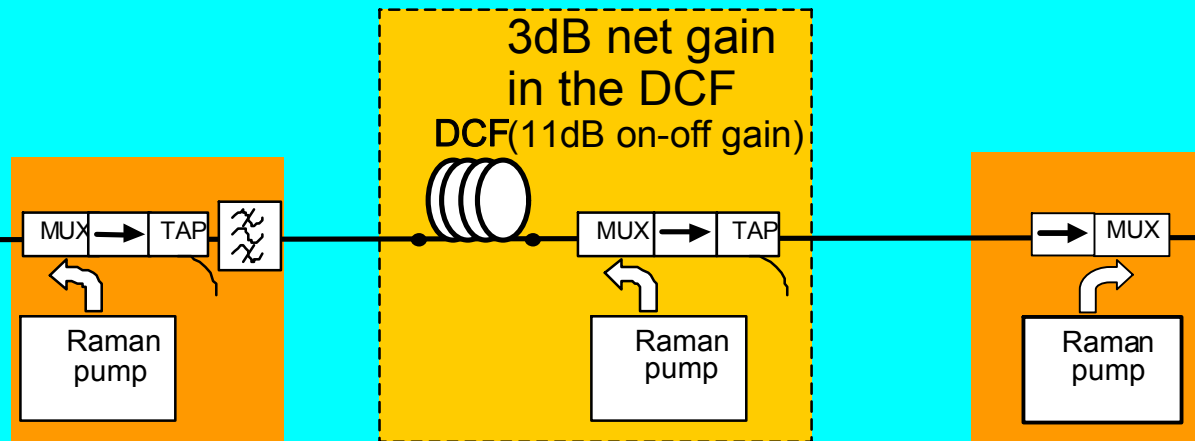
DRA in the link:

31dB on-off Raman gain in the link fiber



DRA in the link & DCF:

21.5dB on-off Raman gain in the link fiber



Criteria for performance assessment (ULH)

Final impairment of the amplifier on the system:

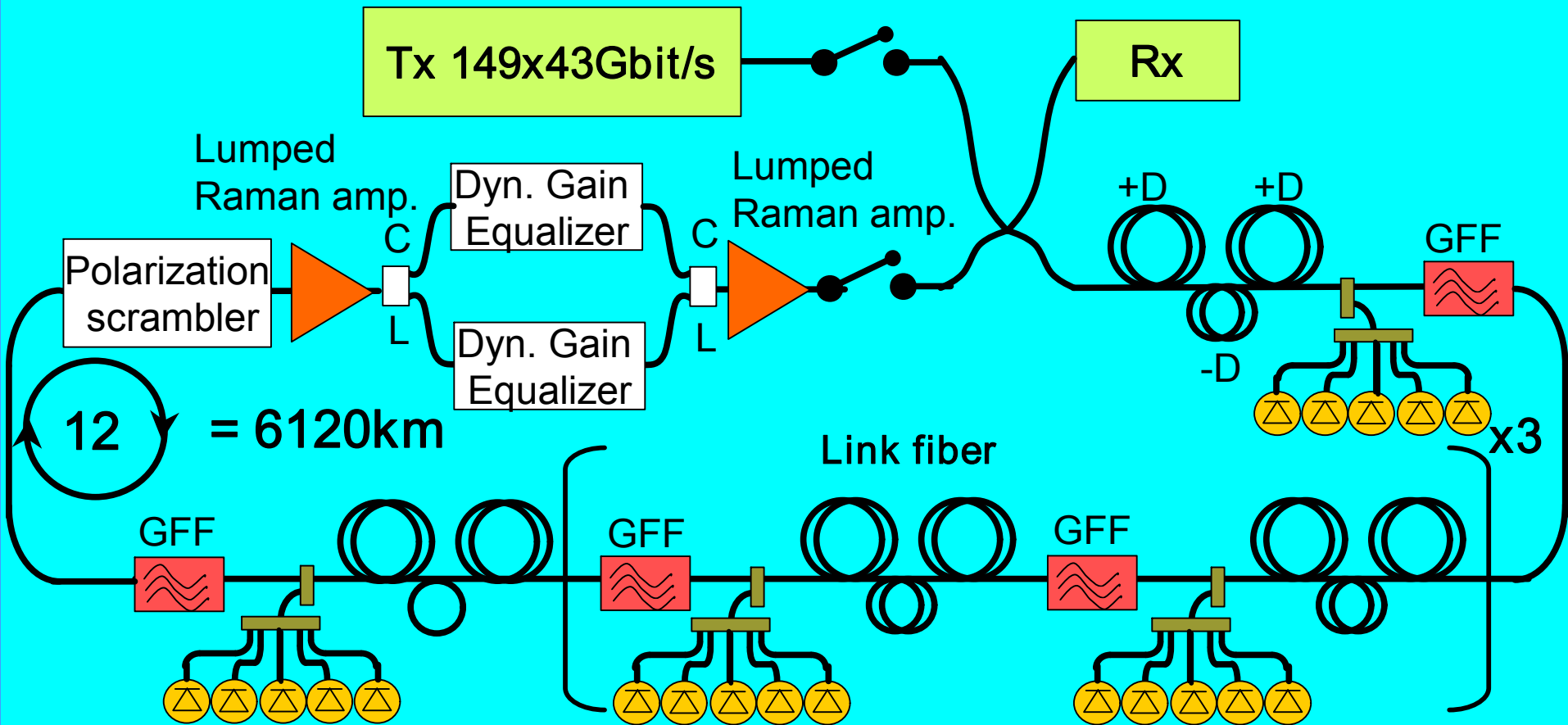
Generation of noise $C_{noise} = N_{ASE} B_{elec} + \frac{1}{2} * \frac{5}{9} \cdot R_{DRS} P_{in}$

Non-linear phase $C_{phase} = \gamma \int_0^L G_{Net}(z) dz$

Achievable distance is proportional to $(C_{noise} C_{phase})^{-1/2}$
→ Parameter $C = C_{noise} \cdot C_{phase}$ (the smaller the better)

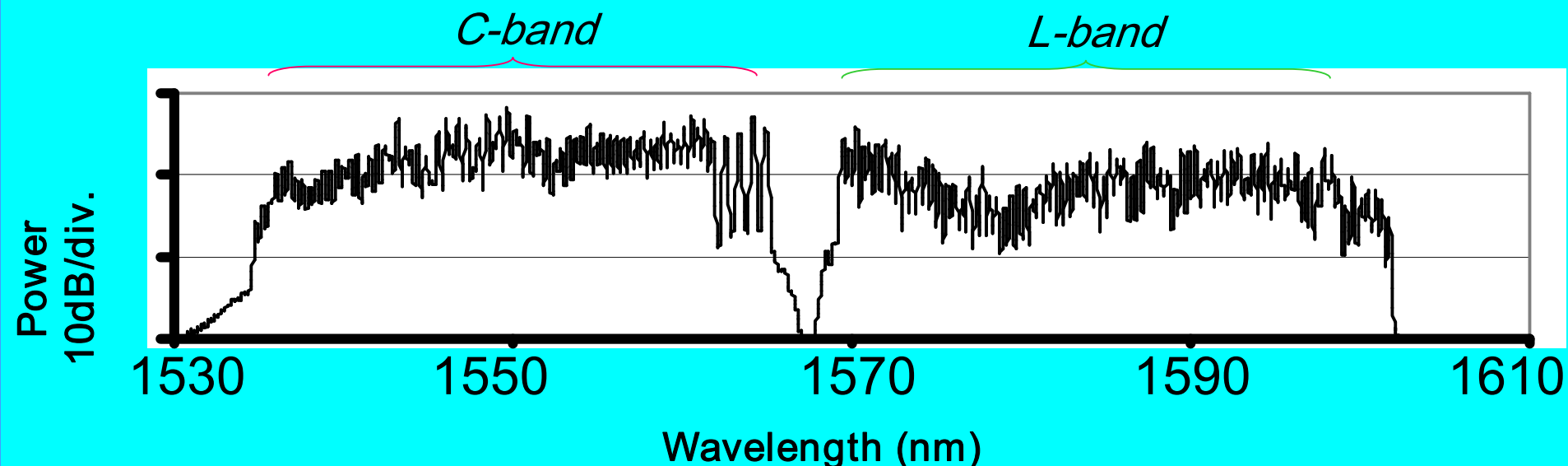
Co-pumping issues to be accounted aside

All-Raman transmission of 6 Tbit/s over 6120 km



All Raman amplification (First+Second order)

Experimental results with all-Raman amplification Spectrum after 6,120km with 149 DPSK channels



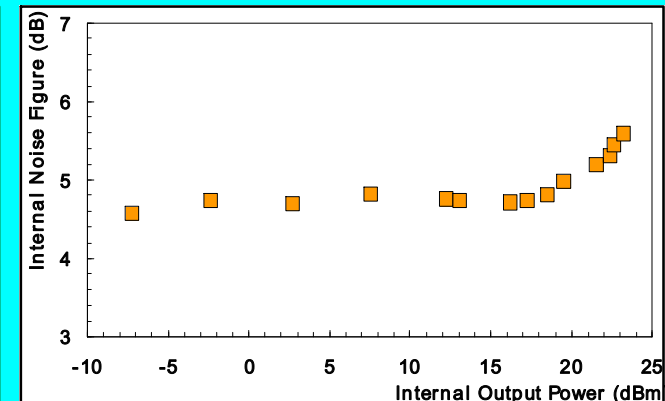
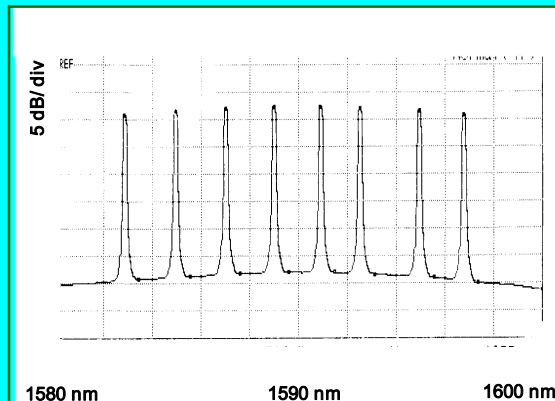
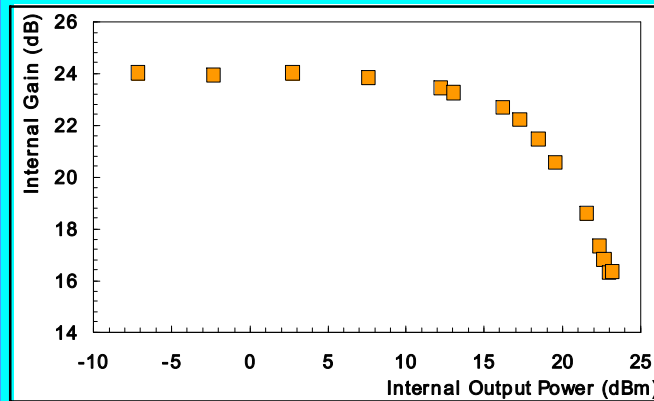
In C-band: more odd than even channels

Gain excursion close to 10 dB after 6120km

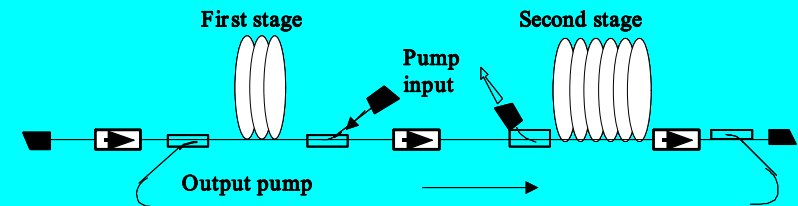
OSNR_{0.1nm} > 16.9dB in L band

OSNR_{0.1nm} > 14.6 dB in C band

Lumped Raman Amplifier



- Use of a specific Raman fiber
 - e.g. Photonic Crystal Fiber
- On-demand gain bandwidth and location
- Weaker sensitivity to signal gain saturation compared to EDFAs
- Robust noise figure in high power input signal regime



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